ADVERSE HIGH RAIL PROFILES: IDENTIFICATION, RISKS AND A SOLUTION

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OUTLINE

- Adverse high rail profiles:
  - What are they?
  - How do we measure them?
  - Why are they a problem?
  - How do they develop?
- A solution: A corrective grinding field test

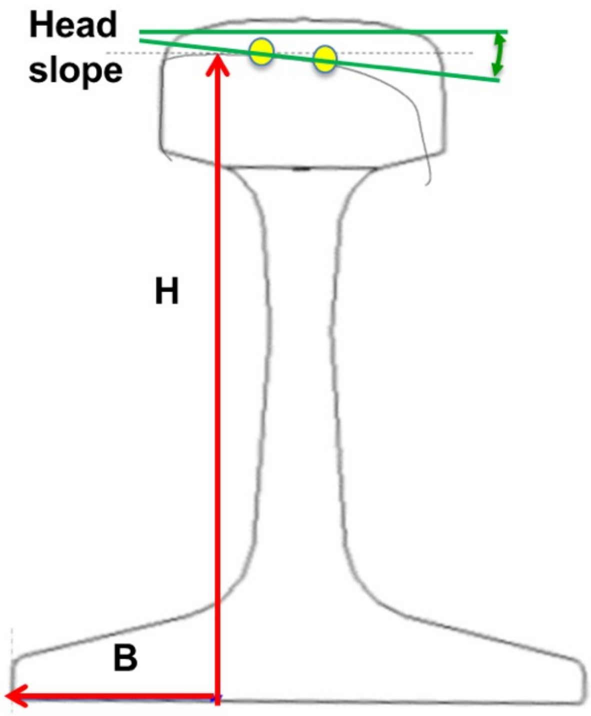
WHAT IS AN ADVERSE HIGH RAIL PROFILE?

- One that shows significant field-side wheel contact

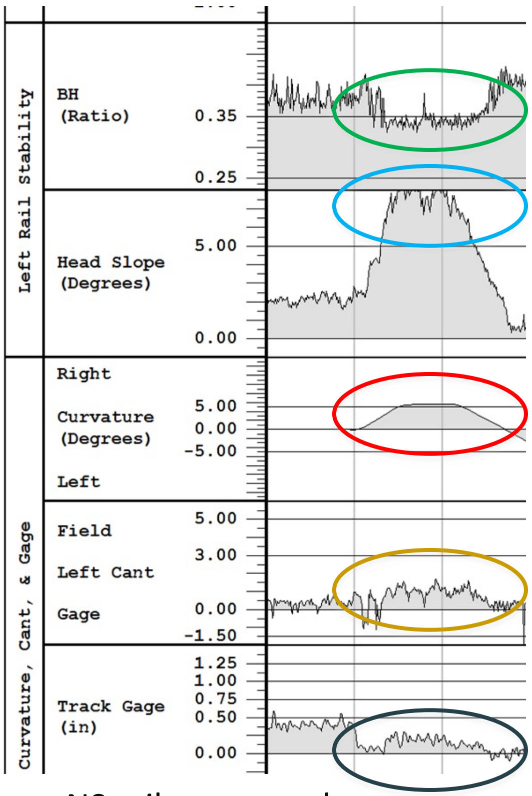
HOW DO WE MEASURE AN ADVERSE HIGH RAIL PROFILE?

- B/H is a ratio that includes
  - H -> the height of the rail at its highest point
  - B -> the horizontal distance between the high point and the field edge of the base
  - New 136# rail: 3” / 7-5/16” = 0.41
  - As high point moves toward field side -> B/H gets smaller
  - Threshold for concern: < 0.35

- Head slope is the angle between horizontal and a line defined by two points one-half inch on either side of rail centerline
  - Steeper slope -> more likely that wheels will run on the field side
  - Threshold for concern: > 5^{o}

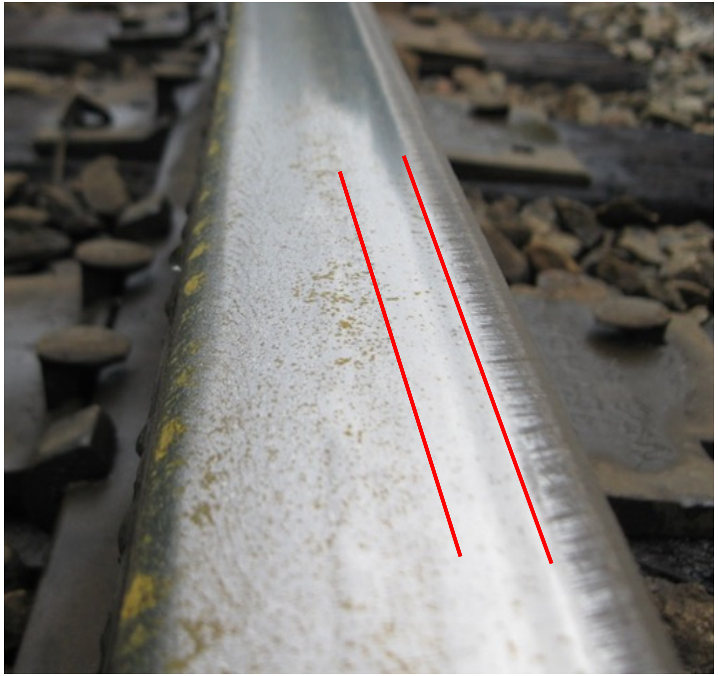


EXAMPLE OF AN ADVERSE HIGH RAIL PROFILE



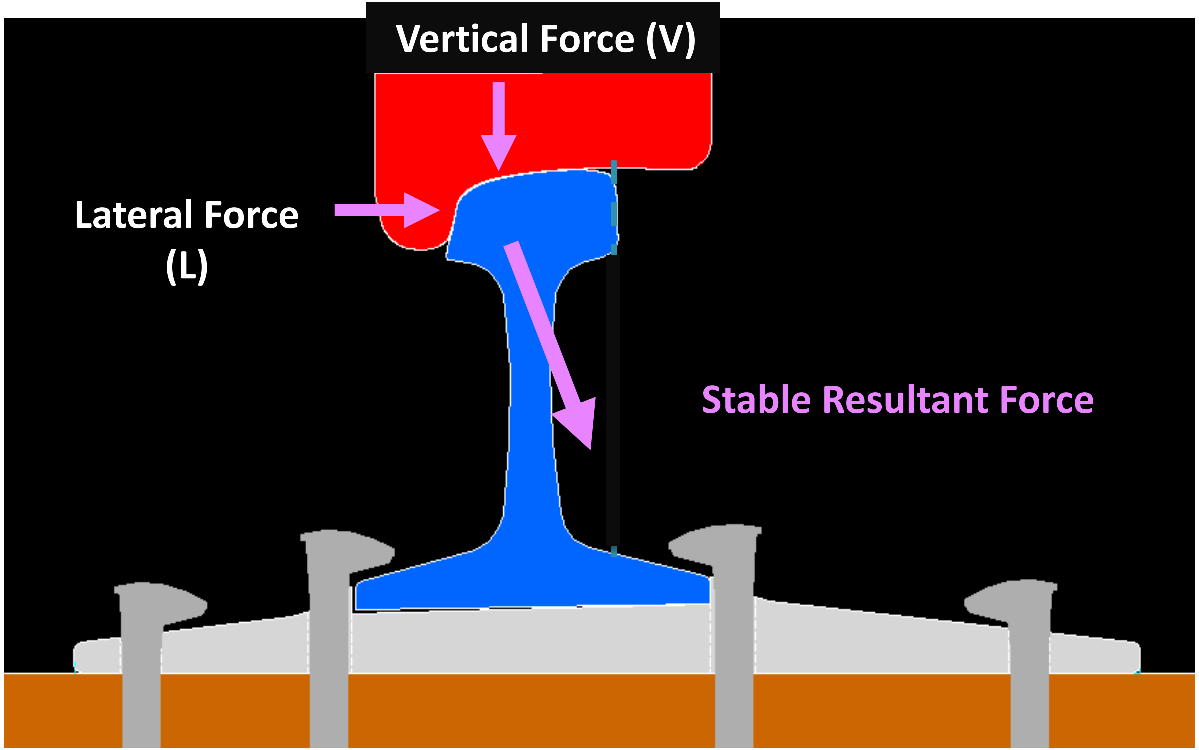
NS rail wear graph

- B/H 0.34
- Head slope 8^o
- Curvature 5^o
- Rail cant 1^o
- Gage ¼”, or 56-3/4”



Primary contact band is on field side

WHEEL / RAIL FORCE DIAGRAM

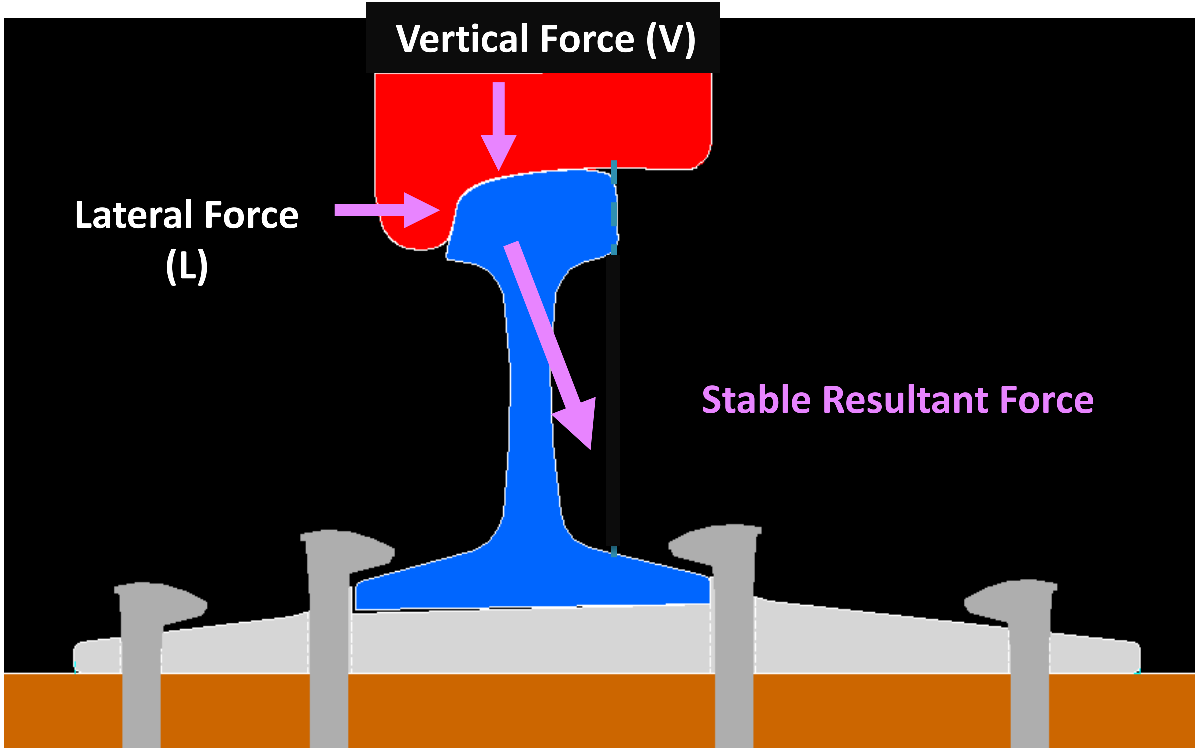


Stable condition

- Lateral & vertical forces produce a resultant directed inside the rail base
- The rail will not roll outward

VIDEO – STABLE HIGH RAIL

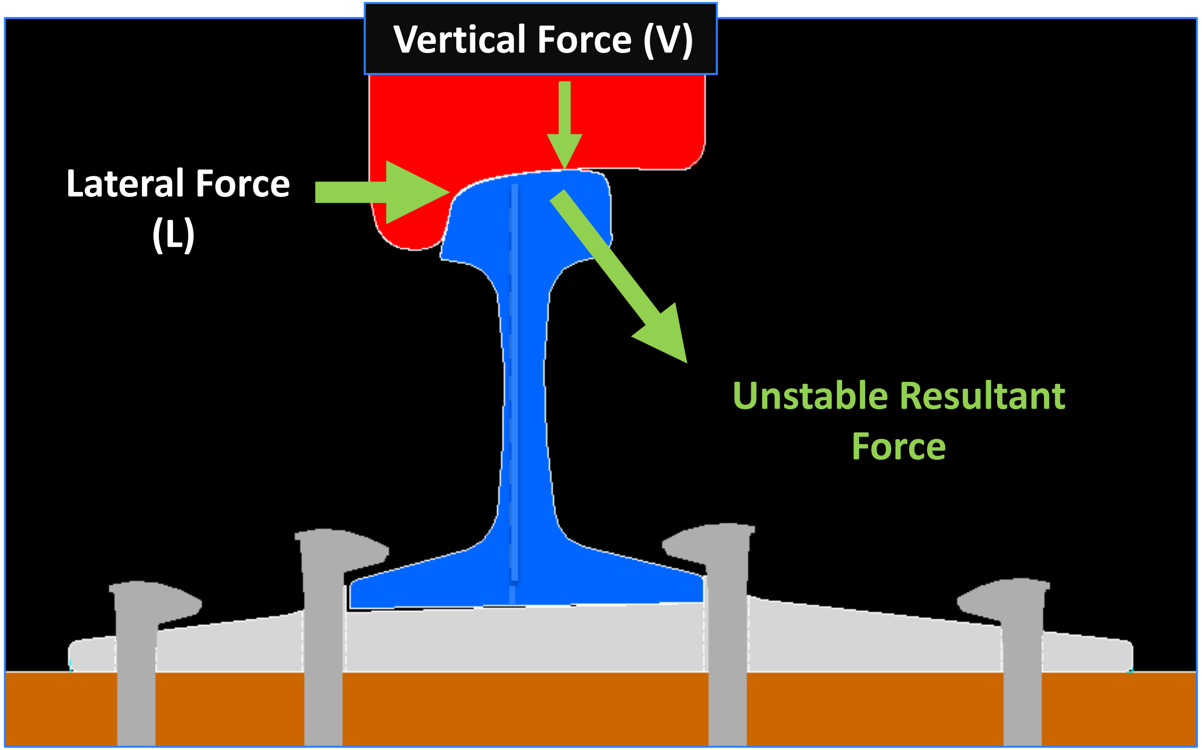
WHEEL / RAIL FORCE DIAGRAM



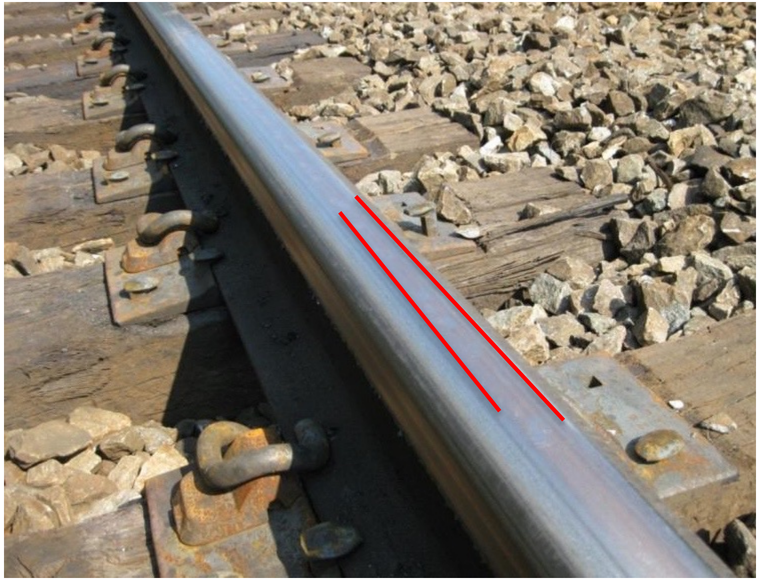
WHEEL / RAIL FORCE DIAGRAM

Unstable condition

- Vertical force has shifted toward the field side
- Lateral force has increased
- Lateral & vertical forces produce a resultant directed outside the rail base
- An unrestrained rail will tend to roll outward



WHAT CAN CAUSE WHEEL CONTACT TO SHIFT?



- The high rail, which had 3^{o} of outward cant because of plate cutting, had the cant removed when the ties were adzed during gaging & fastener replacement.
- The primary wheel contact band shifted toward the field side.

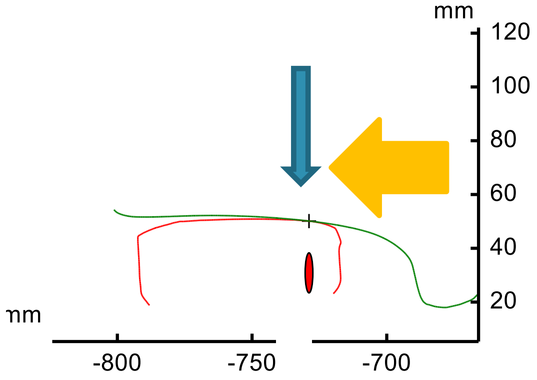
VIDEO SET-UP FOR UNSTABLE LOW RAIL

Same 8° curve; low rail still has conventional tie plates & cut spikes

Anything to be worried about?

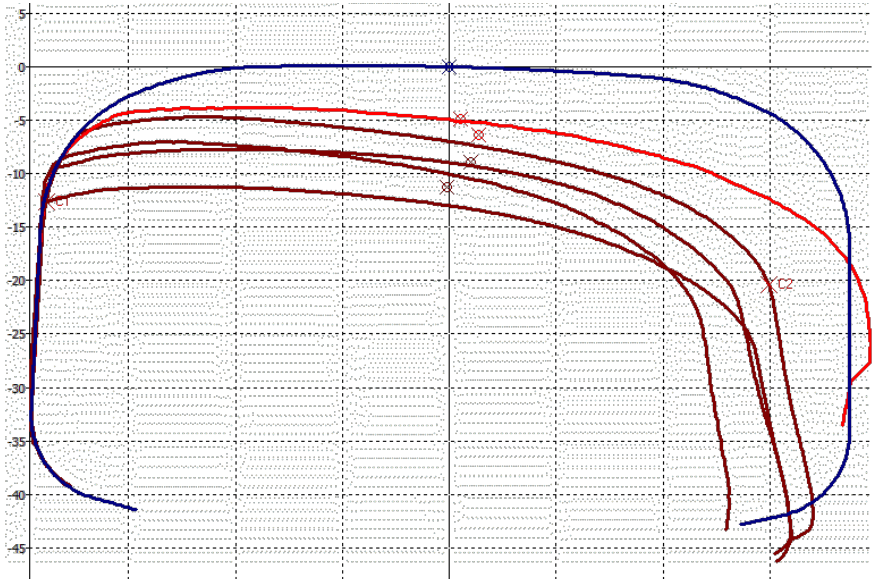
VIDEO - UNSTABLE LOW RAIL

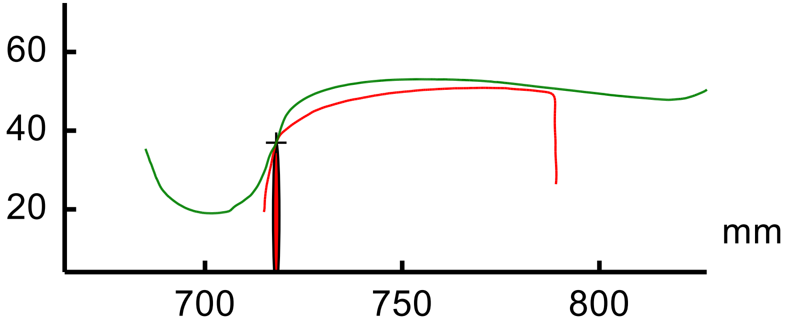
Because of the change in wheel contact on the high rail, the low rail was also subjected to higher lateral forces



WHY IS AN ADVERSE HIGH RAIL PROFILE A PROBLEM?

High rail profiles from five NS rail roll-over derailments (aligned on field side with a new 136RE profile, 1:40 inward cant)





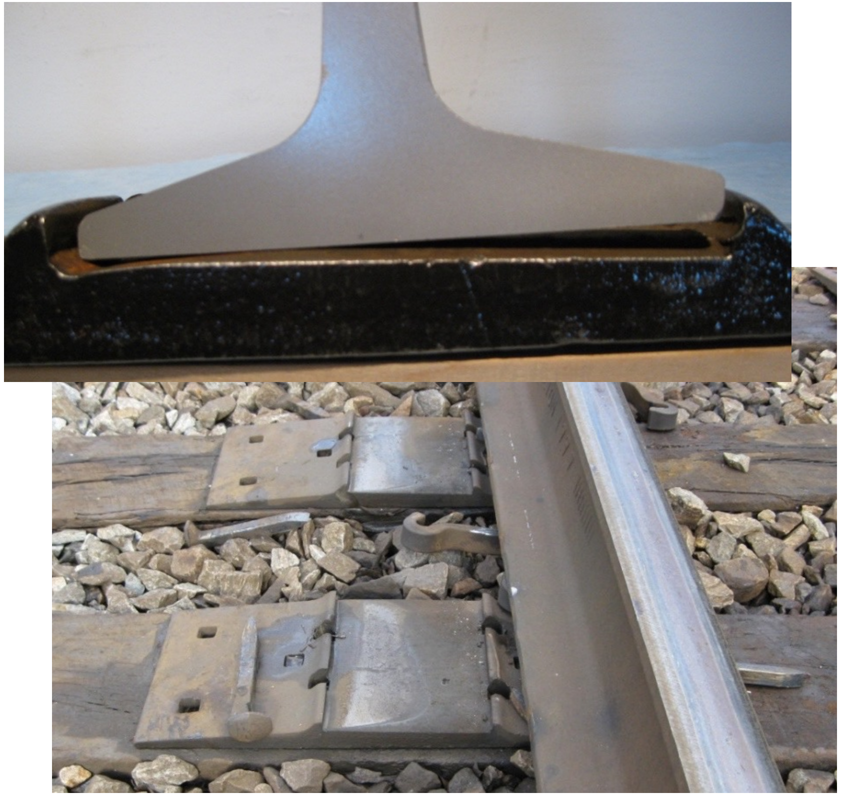
Adverse contact produced by curve-worn rail and 3.5mm hollow-worn wheel. Example of extreme 2-point contact.

Hollow-worn treads are more likely to make field-side contact.

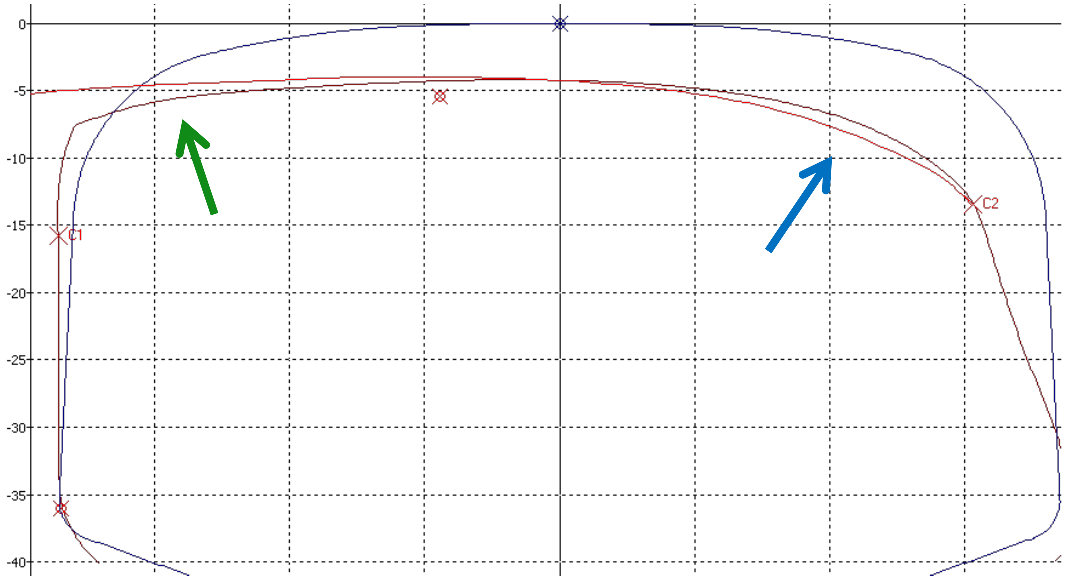
HOW DOES AN ADVERSE HIGH RAIL PROFILE DEVELOP?

Primary reason: Grinding canted rail

Canted rail (on wood ties) is caused by plate-cut ties or worn tie plate rail seats



HOW DOES AN ADVERSE HIGH RAIL PROFILE DEVELOP?



Brown profile: a curve-worn high rail with 3° outward cant

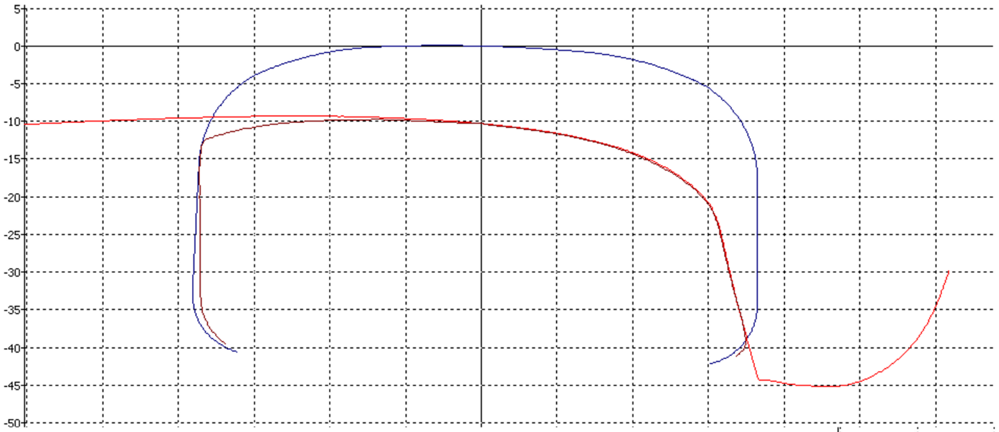
Red profile: high rail template used by Loram & NS

The template can be moved laterally & vertically, but it cannot be rotated

What grinding will result?

Significant grinding on the gage side but no grinding on the field side

WHY IS AN ADVERSE HIGH RAIL PROFILE A PROBLEM?

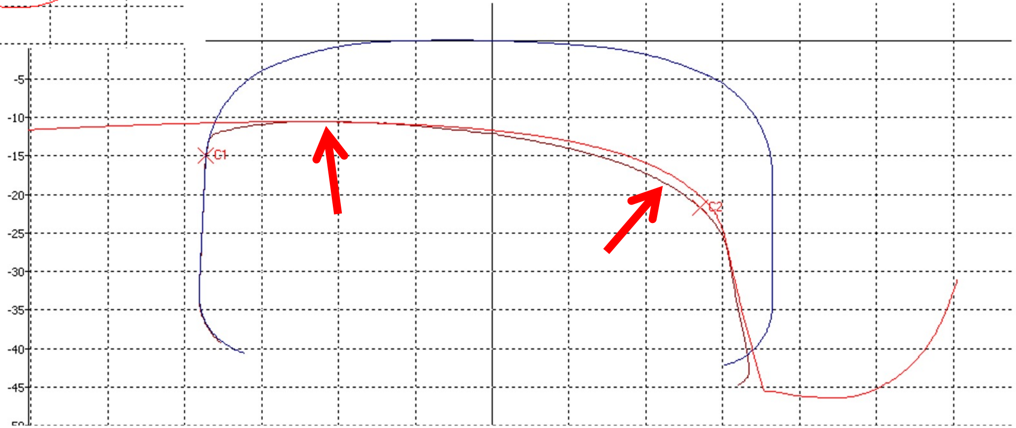


Below: The same slightly-worn wheel and curve-worn rail, but the rail has been set up to 0˚ cant.

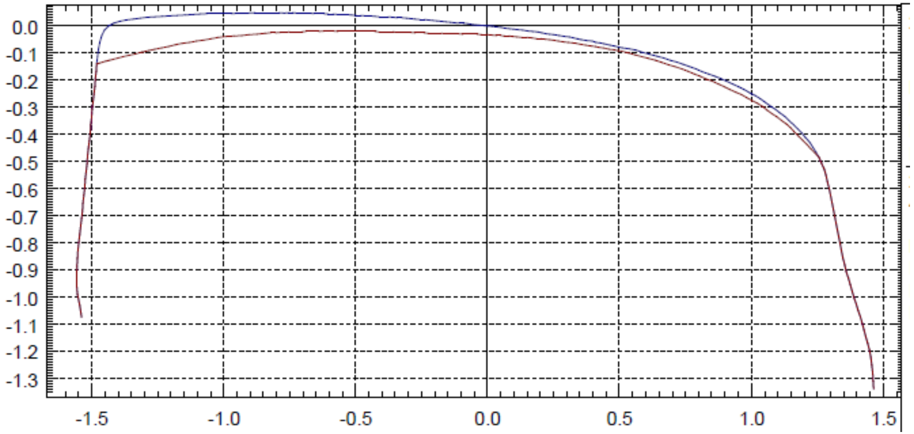
Result: Wheel tread contact has moved toward field side. This is two-point contact, which produces higher-resistance curving and increased lateral force.

Above: A slightly-worn wheel on curve-worn rail with 3° cant

This is conformal contact, which produces favorable wheelset steering



AN EXAMPLE OF HIGH RAIL CORRECTIVE GRINDING



High rail of a 6° curve. The blue profile is pre-grind, and the brown profile is post-grind. A full 1/8-inch was ground off the field-side corner. Both profiles have been rotated to 0° cant.

The same high rail several days after grinding. The primary wheel contact band was moved toward the gage side. Enough metal was removed from the field side to maintain gage-side wheel contact even after the rail was gaged.

CORRECTING ADVERSE HIGH RAIL PROFILES….

- Improves wheelset steering by moving wheel contact toward the gage corner (and take advantage of the larger rolling radius closer to the wheel flange)
- Reduces rail wear, rolling contact fatigue and gage widening
- Improves rail stability by reducing field-side wheel contact

CORRECTIVE GRINDING FIELD TEST

Objective: Correct adverse high rail profiles using NS's normal grinding program.

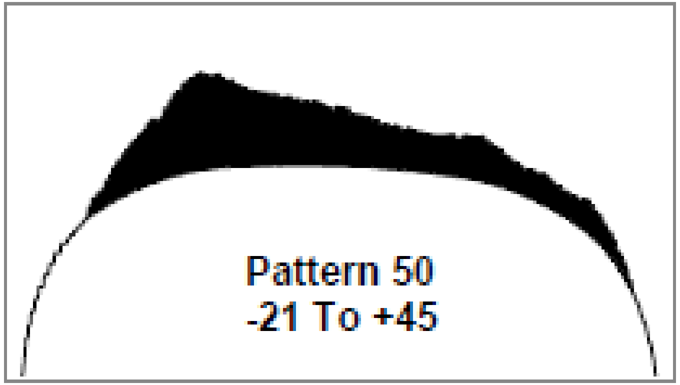
Guidelines: Loram & NS agreed that the number of passes for each curve should be dictated by the metal removal required to correct the worst RCF. The high rail reprofiling would therefore not add time to the grinding schedule.

Plan: Conduct a field test using grinding patterns recommended by Loram

CORRECTIVE GRINDING FIELD TEST - PHASE 1

- Former N&W main line between Roanoke, VA and Bluefield, WV
- Pre-grind inspection included photos of wheel contact location
- Grind patterns
  - For single pass curves, Loram developed a new pattern 50
  - For three-pass curves, Loram selected pattern sequence 22-28-7
- Loram inserted these patterns manually into the RG 417’s grind plan
- Post-grind inspection evaluated changes in wheel contact location

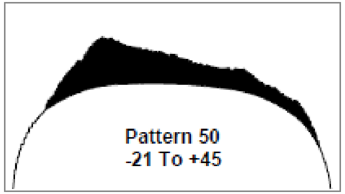
LORAM'S SHADOW DIAGRAMS



Gage side

- Show the relative amount of metal removed across the rail head of a new rail.
- Gage side is always on the right
- The numbers on the bottom line (-21 to +45) indicate the range of grinding stone angles for that pattern
- This newly-developed pattern 50 emphasizes metal removal from the field side

PHASE 1 TEST RESULTS - SINGLE PASS

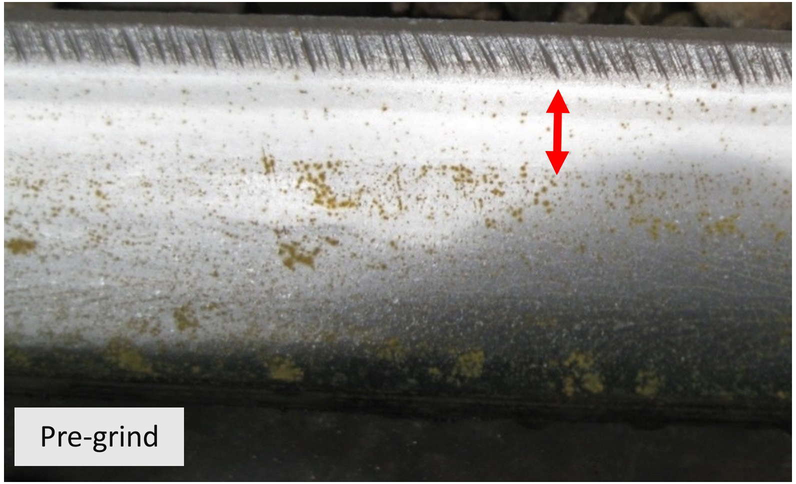


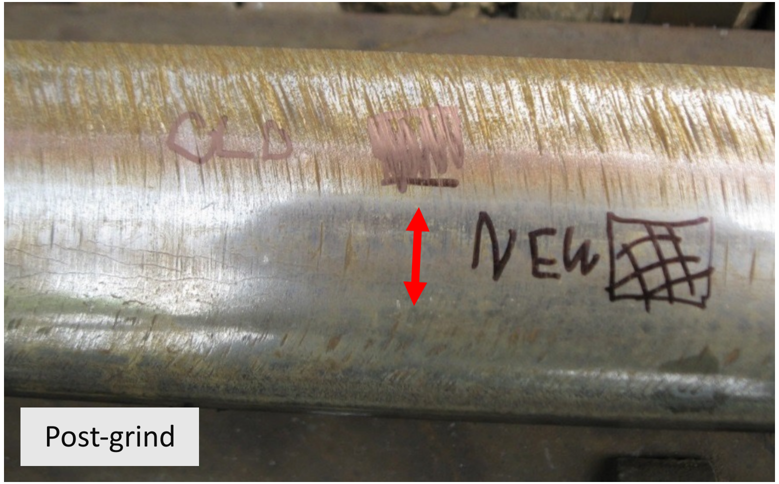
Speed 6 mph

Pre-grind: Primary contact band is on the field side

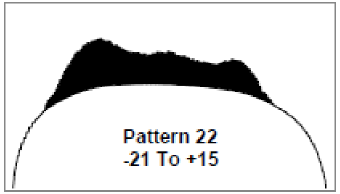
Side wear 6/16“, cant 1.5°, B/H 0.34, head slope 8°

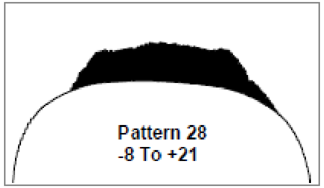
Post grind: Wheel contact shifted toward gage side

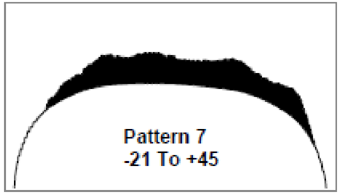




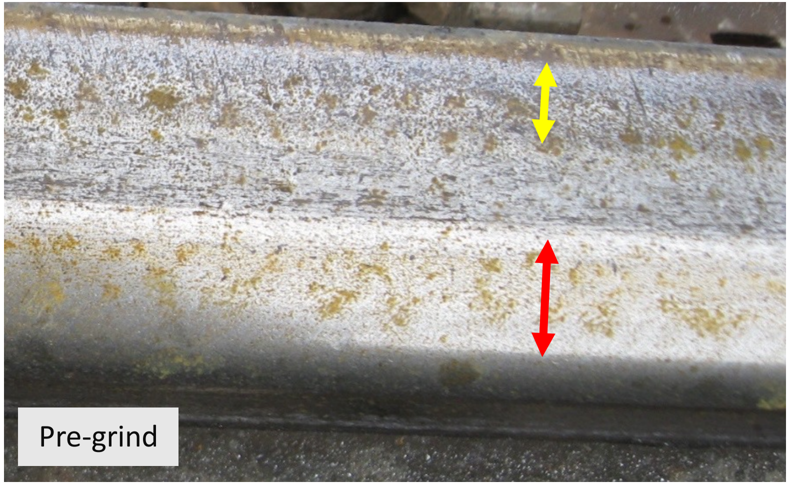
PHASE 1 TEST RESULTS - 3 PASSES







Speed 13 mph for all 3 passes



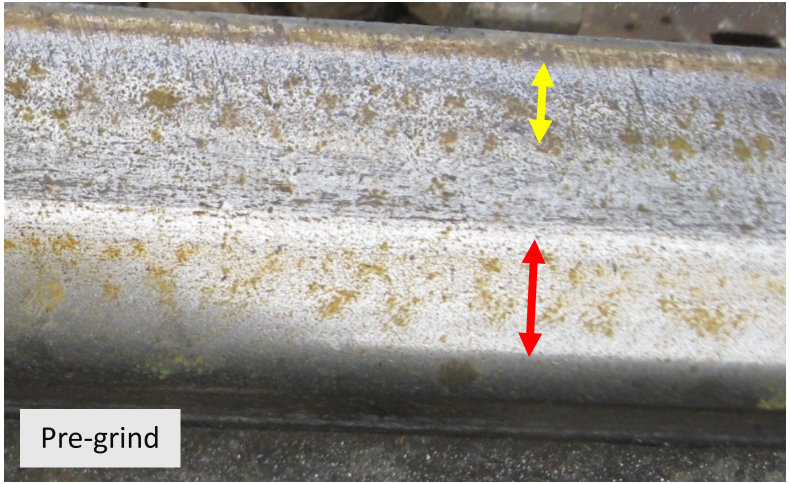
Pre-grind: Primary contact appears to be on gage side (red arrow). There is some field-side wheel contact (yellow arrow), though still-visible grinding marks suggest wheel frequency is low.

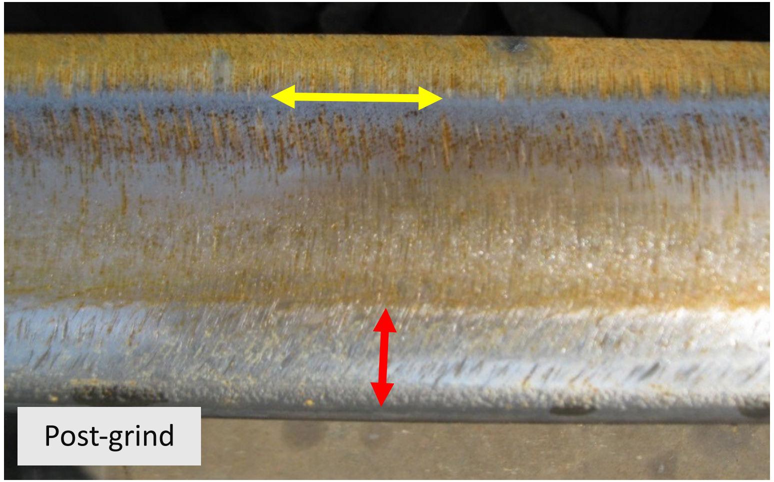
Side wear 6/16“, cant 1^{o}, B/H 0.35, head slope 6^{o}.

PHASE 1 TEST RESULTS - 3 PASSES

Post grind: After 3 passes, the primary wheel contact band is more concentrated on the gage corner (red arrow).

Field-side contact by hollow-tread wheels is still apparent (yellow arrow).

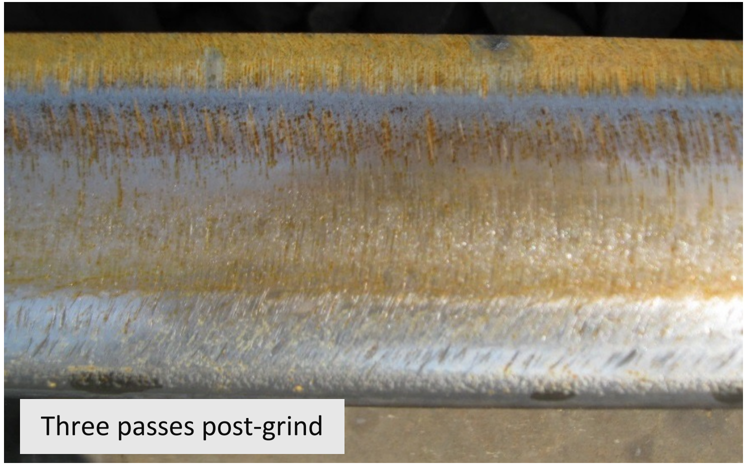




PHASE 1 CONCLUSIONS

- We demonstrated that we could modify an adverse high rail profile and shift wheel contact using our scheduled grinding program.
- On curves that received a single pass, pattern 50 worked well.
- On curves that received three passes, the 22-28-7 sequence did not shift wheel contact as we hoped.
- We agreed that a second field test was needed.

One pass post-grind

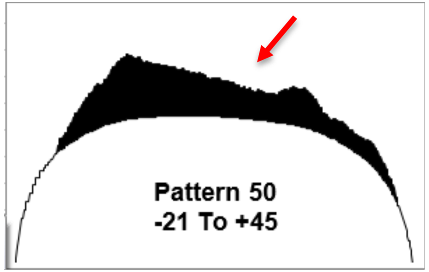


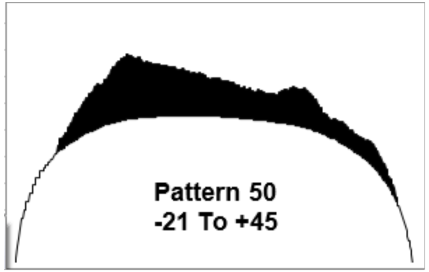
Three passes post-grind

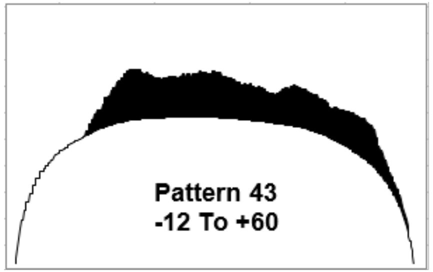
CORRECTIVE GRINDING FIELD TEST - PHASE 2

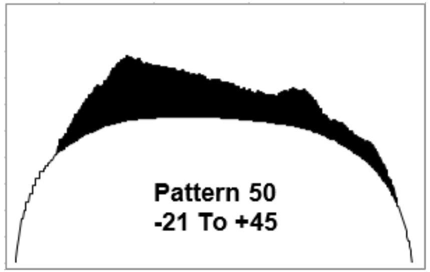
For Phase 2, Loram

- modified pattern 50 to remove more metal between +5° and +15° to address cracks in the gage corner
- changed the 3-pass sequence to patterns 50-43-50.





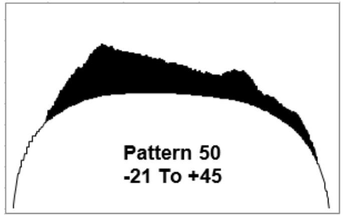




Test location:

- We selected former Southern Railway main between Manassas & Riverton Jct, VA

PHASE 2 TEST RESULTS – SINGLE PASS

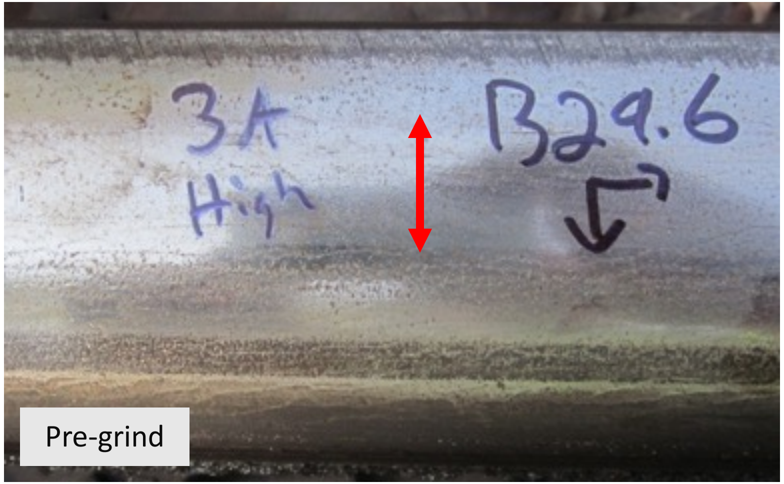


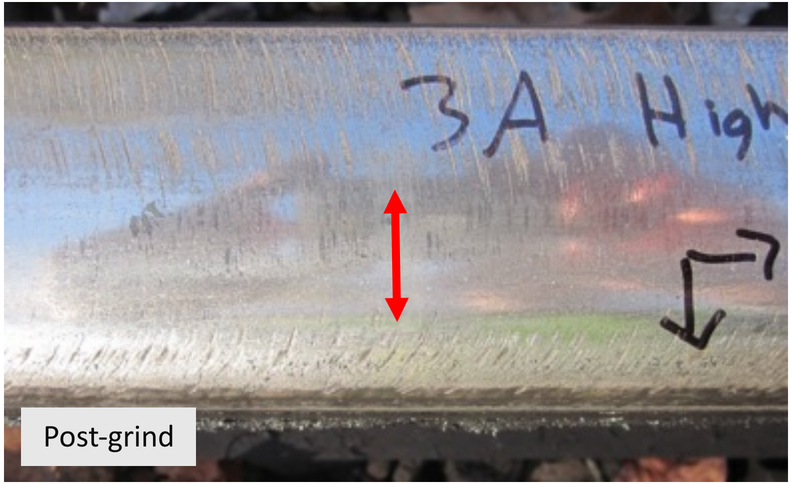
Speed 6 mph

Pre-grind: Primary wheel contact is at the center, though there is evidence of wheel contact over most of the head

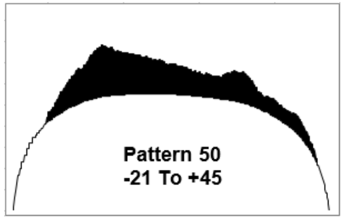
Side wear 7/16", cant 0^o, B/H 0.35, head slope 8^o

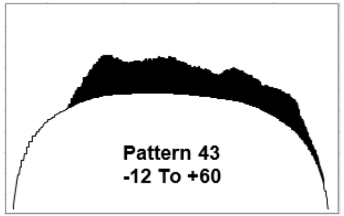
Post-grind: Primary wheel contact has shifted toward the gage side

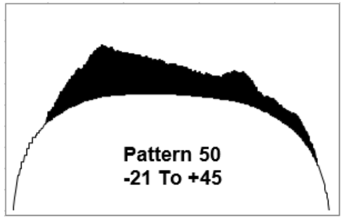




PHASE 2 TEST RESULTS - 3 PASSES







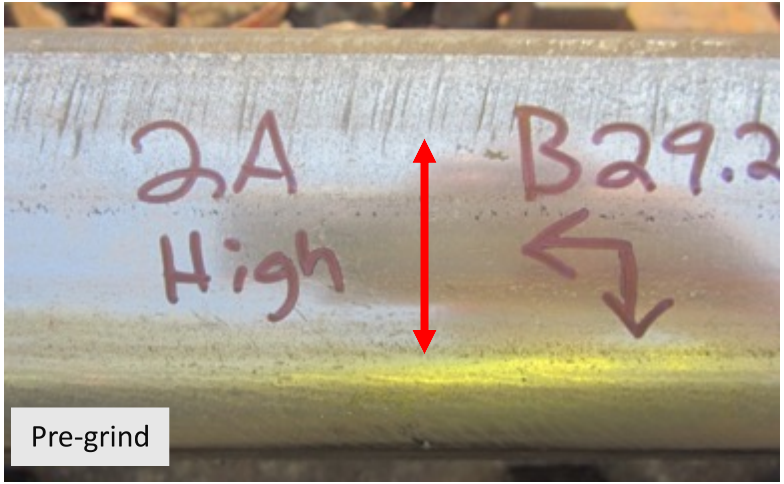
Speed 10 mph for all 3 passes

Pre-grind: Primary wheel contact is at the center, though there is significant wheel contact over most of the head

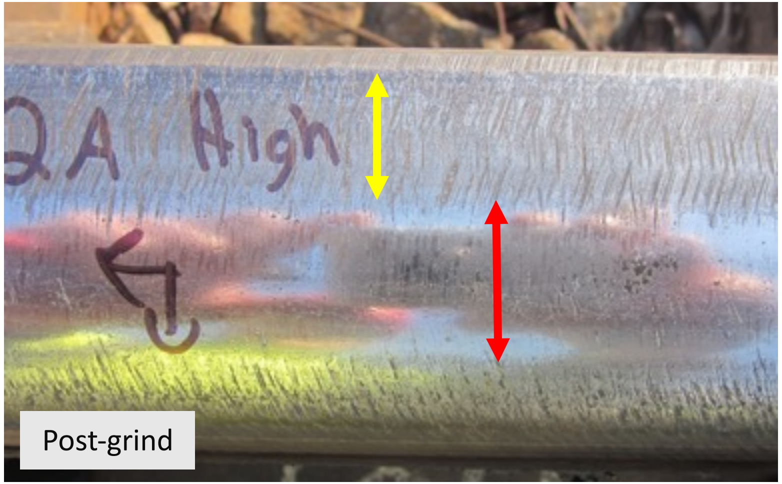
Side wear 7/16“, cant 0^{o}, B/H 0.35, head slope 8^{o}

PHASE 2 TEST RESULTS - 3 PASSES

Post-grind: Primary wheel contact has shifted to the gage side of center. Some hollow-tread wheel contact is still evident on the field half of the head (yellow arrow).



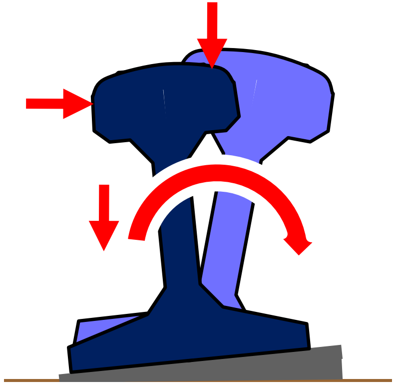
Pre-grind



Post-grind

CONCLUSIONS

1. Curves ground with either the single or 3-pass patterns exhibited a perceptible shift in wheel contact toward the gage side.
2. Field side wheel contact was reduced.



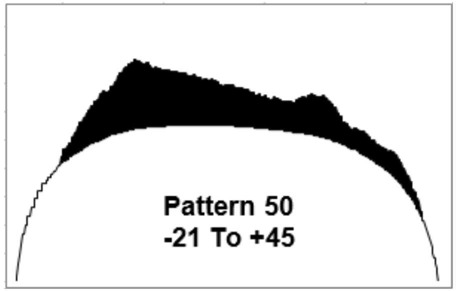
Both observations are significant:

A gage-side shift of the primary contact band indicates that a majority of wheels are taking advantage of a greater rolling radius nearer the flange.

A reduction in field-side contact of hollow-tread wheels suggests a similar steering advantage, but more importantly, indicates that fewer wheels are rolling in a position to cause rail stability problems.

CONCLUSIONS

3. The single pattern 50 high rails exhibit more desirable wheel contact bands than the 3-pass 50-43-50 rails.
4. Curves with significant sidewear (> 6/16”) showed a smaller wheel shift. This may have to do with the fact that increased sidewear is accompanied by increased head slope.
5. Multiple cycles will be needed to accomplish the wheel shift objective (which is primary contact on the gage side and minimal contact on the field side).



NEXT STEPS

1. NS is applying this corrective grinding system-wide. Local M/W managers are using the wear graphs to identify curves with adverse high rail profiles (head slope > 5°).
2. High rails with adverse profiles will get a single pass with pattern 50 at 6 mph.
3. Loram is adding this pattern to the grind plan manually.
4. NS will eventually automate the identification of adverse profiles.

QUESTIONS?